# A NEW PROCEDURE FOR DESIGNING SINGLE SAMPLING PLAN INDEXED THROUGH TRIGNOMETRIC RATIOS 

P.R DIVYA*<br>*Assistant Professor in Statistics, Department of Statistics, Vimala College, Thrissur, Kerala, divyastat@gmail.com

## ABSTRACT

Acceptance Sampling is the methodology which deals with procedures through which decisions to accept or reject of a lot which are based on the result of inspection of samples. The foundation of the scheme of acceptance sampling has laid by Dodge and Romig (1959). General procedures and necessary tables are provided for the selection of single sampling plan through tangent angle as proposed by Norman Bush (1953). Mandelson (1962) has explained the desirability for developing a system of sampling plans indexed through MAPD. Mayer (1967) has explained that the quality standard that the MAPD can be considered as a quality level with other conditions to specify the OC curve. Soundararajan (1975) has constructed tables for selection of single sampling plan indexed through MAPD and K ( $\mathrm{p}_{\mathrm{T}} / \mathrm{p}_{*}$ ) Suresh and Ramkumar (1996) have studied the selection of single sampling plan indexed through Maximum Allowable Average Outgoing Quality (MAAOQ) and MAPD.

This paper provides a new procedure for designing a single sampling plan indexed through trigonometric ratios, hypotenuse ratios along with decision region $\left(d_{1}\right)$ and probabilistic region $\left(d_{2}\right)$ which is more applicable in practical situations. Numerical illustrations are also provided for the construction and selection of the plan parameters using trigonometric ratios and hypotenuse ratios.

Key Words: Single Sampling Plan, Decision Region, Operating Characteristic Curve, Trigonometric ratios

## Introduction

Acceptance Sampling is defined as the procedure for inspection and classification of sample of units selected at random from a larger lot and ultimate decision about the disposition of the lot is made. Basically the "acceptance quality control" system that was developed encompasses the concept of protecting the consumer from getting unacceptable defective product, and encouraging the producer in the use of process quality control through varying the quantity and severity of acceptance inspections in direct relation to the importance of the characteristics inspected, and the inverse relation to the goodness of the quality level as indication of those inspections.

The single sampling plan is the most widely used basic sampling plan in the area of acceptance sampling. The performance of a sampling plan is identified through an OC curve. For designing a sampling inspection plan, it is the usual practice to consider the OC curve passes through any two of the quality levels. Mandelson (1962) has explained the desirability for developing such a system of sampling plans indexed through MAPD Mayer (1967) has explained that the quality standard that the MAPD can be considered as a quality level along with other conditions to specify an OC curve. Soundararajan (1975) has constructed tables for selection of single sampling plan indexed through MAPD and
$\mathrm{K}=\frac{p_{T}}{p_{*}}$.Suresh and Ramkumar (1996) have studied the selection of single sampling plan indexed through Maximum Allowable Average Outgoing Quality (MAAOQ).

This paper provides a new procedure for designing attribute single sampling plan indexed through trigonometric ratios and hypotenuse ratios. Also considering the ability of the declination angles of the tangent at the inflection point on the OC curve for discrimination of the Single Sampling Plan (SSP)
Here, $\tan \theta_{1}=\frac{0.95-L\left(p_{*}\right)}{d_{1}}$
From (1) one can find ( $\mathrm{n}, \mathrm{c}$ ) for a particular $\mathrm{L}(\mathrm{p} *)$ and $\mathrm{d}_{1}$.So we can state that both $\theta_{1}$ and $\mathrm{d}_{1}$ uniquely determines the SSP.
Similarly, $\tan \theta_{2}=\frac{L\left(p_{*}\right)-0.10}{d_{2}-d_{1}}$.
From (2) one can find ( $\mathrm{n}, \mathrm{c}$ ) for a particular $\mathrm{L}(\mathrm{p} *)$ and $\left(\mathrm{d}_{2}-\mathrm{d}_{1}\right)$. So we can state that both $\theta_{2}$ and $\left(d_{2}-\mathrm{d}_{1}\right)$ uniquely determines the SSP.
And, $\tan \theta_{3}=\frac{L\left(p_{*}\right)}{d_{2}} \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots$
From (3) one can find ( $\mathrm{n}, \mathrm{c}$ ) for a particular $\mathrm{L}\left(\mathrm{p}_{*}\right)$ and $\mathrm{d}_{2}$. So we can state that both $\theta_{3}$ and $\mathrm{d}_{2}$ uniquely determines the SSP.

From figure1, we have $\triangle \mathrm{ABC}$ represents the approximate area inscribed by the quality levels $p_{1}$ and $p_{*} . \Delta C D E$ represents the approximate area inscribed by the quality levels $p_{*}$ and $p_{2}$.And the $\Delta$ BFG represents the approximate area inscribed by the quality levels $p_{1}$ and $\mathrm{p}_{2 .} \theta_{1}$ is the inscribed triangle by OC with quality levels $\mathrm{p}_{1}$ and $\mathrm{p} * \cdot \theta_{2}$ represent the inscribed triangle by OC with quality levels $\mathrm{p} *$ and $\mathrm{p}_{2}$. And $\theta_{3}$ is the inscribed triangle by $O C$ with quality levels $p_{1}$ and $p_{2}$.

## Fig 1: OC Curve for Decision Region (d1) and Probabilistic Region (d2) and Tangent Angles



## Selection of sampling plans

Table 1 is given for selected values of $c$. Here SSP with $\mathrm{c}=0$ are not considered, since $\mathrm{c}=0$ plans do not involve an inflection point on the OC curve. Tables are given for the values of $\mathrm{L}\left(\mathrm{p}_{*}\right)$ for $\mathrm{c}=1,2, \ldots \ldots 20$.

Table 1: Certain Parametric Values for SSP

| $\mathbf{c}$ | $\left.\mathbf{L}^{\mathbf{(}} \mathbf{p}^{*}\right)$ | $\mathbf{n p}_{\mathbf{1}}$ | $\mathbf{n p}_{\mathbf{2}}$ | $\mathbf{d}_{\mathbf{1}}$ | $\mathbf{d}_{\mathbf{2}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.735759 | 0.355 | 3.89 | 0.645 | 3.535 |
| $\mathbf{2}$ | 0.676676 | 0.818 | 5.322 | 1.182 | 4.504 |
| $\mathbf{3}$ | 0.647232 | 1.366 | 6.681 | 1.634 | 5.315 |
| $\mathbf{4}$ | 0.628837 | 1.97 | 7.994 | 2.03 | 6.024 |
| $\mathbf{5}$ | 0.615961 | 2.613 | 9.275 | 2.387 | 6.662 |
| $\mathbf{6}$ | 0.606303 | 3.286 | 10.532 | 2.714 | 7.246 |
| $\mathbf{7}$ | 0.598714 | 3.981 | 11.771 | 3.019 | 7.79 |
| $\mathbf{8}$ | 0.592547 | 4.695 | 12.995 | 3.305 | 8.3 |
| $\mathbf{9}$ | 0.587408 | 5.426 | 14.206 | 3.574 | 8.78 |
| $\mathbf{1 0}$ | 0.58304 | 6.169 | 15.407 | 3.831 | 9.238 |
| $\mathbf{1 1}$ | 0.579267 | 6.924 | 16.598 | 4.076 | 9.674 |
| $\mathbf{1 2}$ | 0.575965 | 7.69 | 17.782 | 4.31 | 10.092 |
| $\mathbf{1 3}$ | 0.573045 | 8.464 | 18.958 | 4.536 | 10.494 |
| $\mathbf{1 4}$ | 0.570437 | 9.246 | 20.128 | 4.754 | 10.882 |
| $\mathbf{1 5}$ | 0.56809 | 10.035 | 21.292 | 4.965 | 11.257 |
| $\mathbf{1 6}$ | 0.565962 | 10.831 | 22.452 | 5.169 | 11.621 |
| $\mathbf{1 7}$ | 0.564023 | 11.633 | 23.606 | 5.367 | 11.973 |
| $\mathbf{1 8}$ | 0.562245 | 12.442 | 24.756 | 5.558 | 12.314 |
| $\mathbf{1 9}$ | 0.560607 | 13.254 | 25.902 | 5.746 | 12.648 |
| $\mathbf{2 0}$ | 0.559093 | 14.072 | 27.045 | 5.928 | 12.973 |

Using the table it can be noted that as c increased $\mathrm{d}_{1}, \mathrm{~d}_{2}$ increases but $\mathrm{L}(\mathrm{p} *)$ decreases.

## Example 1

For a given sample size $\mathrm{n}=100$ and to attain an area of 0.85 . Find the acceptance to be taken for attain a better OC curve.
Using table 2 we can easily read off, for area $\mathrm{ABC}=0.8549$ the corresponding acceptance number $\mathrm{c}=13$.

## Example 2

For a given sample size $\mathrm{n}=100$ and to attain an area of 1.18 , find the acceptance to be taken for attain a better OC curve.
Using table 3 we can find that for area $\mathrm{CDE}=1.18$, the corresponding acceptance number $\mathrm{c}=7$.

## Example3

For a given sample size $\mathrm{n}=100$ and to attain an area of 3 , find the acceptance to be taken for attain a better OC curve.
Using table 4 we can easily read off, that the appropriate acceptance number is $\mathrm{c}=13$.
Example 4
For an OC curve to which a tangent is drawn, it is specified the operating ratio $\mathrm{R}_{4}=2.2394$. Find the appropriate acceptance number.
Using table 8 it can be seen that the appropriate c for the operating ratio $\mathrm{R}_{4}=2.2394$ is 3.That is $\mathrm{c}=3$.

## Construction of Tables

When the proportion of defective in the lot is small and sample size is large so that $n p<5$ then the lot quality assumed to follow Poisson distribution. The probability of acceptance under Poisson model is given as

$$
\begin{equation*}
\mathrm{L}(\mathrm{p})=\sum_{r=0}^{c} \frac{e^{-n p}(n p)^{r}}{r!} . \tag{4}
\end{equation*}
$$

Where p is the proportion defective of the lot, p coordinate of the inflection point will obtain as $\mathrm{p} *=\frac{c}{n}$.
$\mathrm{L}(\mathrm{p} *)$ represents the probability of acceptance of an utmost satisfactory quality (MAPD)

$$
\begin{equation*}
\mathrm{L}\left(\mathrm{p}_{*}\right)=\sum_{r=0}^{c} \frac{e^{-c}(c)^{r}}{r!} . \tag{5}
\end{equation*}
$$

Thus $L\left(p_{*}\right)$ is a function of $c$ alone, and it is constant for fixed $c$.
From figure, $\tan \theta_{1}=\frac{0.95-L\left(p_{*}\right)}{d_{1}}$, the declination angle $\theta_{1}=\tan ^{-1}\left(\frac{0.95-L\left(p_{*}\right)}{d_{1}}\right)$. Similarly $\tan \theta_{2}=\frac{L\left(p_{*}\right)-0.10}{d_{2}-d_{1}}$ and the declination angle is $\theta_{2}=\tan ^{-1}\left(\frac{. L\left(p_{*}\right)-0.10}{d_{2}-d_{1}}\right)$.
And $\tan \theta_{3}=\frac{L\left(p_{*}\right)}{d_{2}}$, the declination angle is $\theta_{3}=\tan ^{-1}\left(\frac{. L\left(p_{*}\right)}{d_{2}}\right)$.
For different values of $\mathrm{c}=1,2, \ldots .20, \mathrm{~L}(\mathrm{p} *)$ is determined from equation (5). Substituting the appropriate values in equation (1),(2),(3) for fixed $L(p *), \mathrm{d}_{1}$, $\left(\mathrm{d}_{2}-\mathrm{d}_{1}\right), \mathrm{d}_{2}$ and hence angle $\theta_{1}, \theta_{2}, \theta_{3}$ and ( $\mathrm{n}, \mathrm{c}$ ) are obtained.

Table-2 provides the area of triangle ABC for a fixed n for different values of c . Table-3 provides the area of triangle CDE for a fixed n for different values of c . Table- 4 provides the area of triangle BFG for a fixed n for different values of c Table- 5 provides the operating ratio $R_{1}$ for different values of $c$. Table-6 provides the operating ratio $R_{2}$ for different values of $c$. Table-7 provides the operating ratio $\mathrm{R}_{3}$ for different values of c . Table-8 provides the operating ratio $\mathrm{R}_{4}$.

## Conclusion

MAPD is the quality measure proposed for designing the sampling plan. MAPD has evolved as a world wide accepted quality measure to discriminate between good and bad lots. Many procedures for designing single sampling plan have been developing over years using MAPD as quality index. When sampling procedure fails to obtain OC curve which lies closer to the ideal one. MAPD related plans which are more efficient for achieving better quality products. Therefore Quality parameters like trigonometric ratio's, hypotenuse ratio's decision region $\left(\mathrm{d}_{1}\right)$, probabilistic region $\left(\mathrm{d}_{2}\right)$ which are more applicable in suitable situations.

Table 2: The area of triangle ABC for a fixed $n$

| $\mathbf{c}$ | $\mathbf{d}_{\mathbf{1}}$ | $\mathbf{L}\left(\mathbf{p}^{*}\right)$ | $\mathbf{. 9 5}-\mathbf{L}\left(\mathbf{p}^{*}\right)$ | $\mathbf{A C}$ | areaABC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.645 | 0.7358 | 0.2142 | 0.6797 | 0.0691 |
| $\mathbf{2}$ | 1.182 | 0.6767 | 0.2733 | 1.2132 | 0.1615 |
| $\mathbf{3}$ | 1.634 | 0.6472 | 0.3028 | 1.6618 | 0.2474 |
| $\mathbf{4}$ | 2.03 | 0.6288 | 0.3212 | 2.0552 | 0.3260 |
| $\mathbf{5}$ | 2.387 | 0.6160 | 0.3340 | 2.4103 | 0.3987 |
| $\mathbf{6}$ | 2.714 | 0.6063 | 0.3437 | 2.7357 | 0.4664 |
| $\mathbf{7}$ | 3.019 | 0.5987 | 0.3513 | 3.0394 | 0.5303 |
| $\mathbf{8}$ | 3.305 | 0.5925 | 0.3575 | 3.3243 | 0.5907 |
| $\mathbf{9}$ | 3.574 | 0.5874 | 0.3626 | 3.5923 | 0.6480 |
| $\mathbf{1 0}$ | 3.831 | 0.5830 | 0.3670 | 3.8485 | 0.7029 |
| $\mathbf{1 1}$ | 4.076 | 0.5793 | 0.3707 | 4.0928 | 0.7556 |
| $\mathbf{1 2}$ | 4.31 | 0.5760 | 0.3740 | 4.3262 | 0.8060 |
| $\mathbf{1 3}$ | 4.536 | 0.5730 | 0.3770 | 4.5516 | 0.8549 |
| $\mathbf{1 4}$ | 4.754 | 0.5704 | 0.3796 | 4.7691 | 0.9022 |
| $\mathbf{1 5}$ | 4.965 | 0.5681 | 0.3819 | 4.9797 | 0.9481 |
| $\mathbf{1 6}$ | 5.169 | 0.5660 | 0.3840 | 5.1832 | 0.9925 |
| $\mathbf{1 7}$ | 5.367 | 0.5640 | 0.3860 | 5.3809 | 1.0358 |
| $\mathbf{1 8}$ | 5.558 | 0.5622 | 0.3878 | 5.5715 | 1.0776 |
| $\mathbf{1 9}$ | 5.746 | 0.5606 | 0.3894 | 5.7592 | 1.1187 |
| $\mathbf{2 0}$ | 5.928 | 0.5591 | 0.3909 | 5.9409 | 1.1586 |

Table 3: The area of triangle CDE for a fixed $n$

| $\mathbf{c}$ | $\mathbf{d 2} \mathbf{- d 1}$ | $\mathbf{L}\left(\mathbf{p}^{*}\right)$ | $\mathbf{L}\left(\mathbf{p}^{*}\right) \mathbf{- . 1 0}$ | $\mathbf{C E}$ | area CDE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 2.89 | 0.73576 | 0.6358 | 2.9591 | 0.9187 |
| $\mathbf{2}$ | 3.322 | 0.67668 | 0.5767 | 3.3717 | 0.9579 |
| $\mathbf{3}$ | 3.681 | 0.64723 | 0.5472 | 3.7215 | 1.0072 |
| $\mathbf{4}$ | 3.994 | 0.62884 | 0.5288 | 4.0289 | 1.0561 |
| $\mathbf{5}$ | 4.275 | 0.61596 | 0.5160 | 4.3060 | 1.1029 |
| $\mathbf{6}$ | 4.532 | 0.6063 | 0.5063 | 4.5602 | 1.1473 |
| $\mathbf{7}$ | 4.771 | 0.59871 | 0.4987 | 4.7970 | 1.1897 |
| $\mathbf{8}$ | 4.995 | 0.59255 | 0.4925 | 5.0192 | 1.2301 |
| $\mathbf{9}$ | 5.206 | 0.58741 | 0.4874 | 5.2288 | 1.2687 |
| $\mathbf{1 0}$ | 5.407 | 0.58304 | 0.4830 | 5.4285 | 1.3059 |
| $\mathbf{1 1}$ | 5.598 | 0.57927 | 0.4793 | 5.6185 | 1.3415 |
| $\mathbf{1 2}$ | 5.782 | 0.57597 | 0.4760 | 5.8016 | 1.3760 |
| $\mathbf{1 3}$ | 5.958 | 0.57304 | 0.4730 | 5.9767 | 1.4092 |
| $\mathbf{1 4}$ | 6.128 | 0.57044 | 0.4704 | 6.1460 | 1.4414 |
| $\mathbf{1 5}$ | 6.292 | 0.56809 | 0.4681 | 6.3094 | 1.4726 |
| $\mathbf{1 6}$ | 6.452 | 0.56596 | 0.4660 | 6.4688 | 1.5032 |
| $\mathbf{1 7}$ | 6.606 | 0.56402 | 0.4640 | 6.6223 | 1.5327 |
| $\mathbf{1 8}$ | 6.756 | 0.56224 | 0.4622 | 6.7718 | 1.5615 |
| $\mathbf{1 9}$ | 6.902 | 0.56061 | 0.4606 | 6.9174 | 1.5896 |
| $\mathbf{2 0}$ | 7.045 | 0.55909 | 0.4591 | 7.0599 | 1.6172 |

Table 4: The area of triangle BFG for a fixed $n$

| $\mathbf{c}$ | $\mathbf{L}\left(\mathbf{p}^{*}\right)$ | $\mathbf{d 2}$ | $\mathbf{F G}$ | area BFG |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.7358 | 3.535 | 3.611 | 1.300 |
| $\mathbf{2}$ | 0.6767 | 4.504 | 4.555 | 1.524 |
| $\mathbf{3}$ | 0.6472 | 5.315 | 5.354 | 1.720 |
| $\mathbf{4}$ | 0.6288 | 6.024 | 6.057 | 1.894 |
| $\mathbf{5}$ | 0.6160 | 6.662 | 6.690 | 2.052 |
| $\mathbf{6}$ | 0.6063 | 7.246 | 7.271 | 2.197 |
| $\mathbf{7}$ | 0.5987 | 7.79 | 7.813 | 2.332 |
| $\mathbf{8}$ | 0.5925 | 8.3 | 8.321 | 2.459 |
| $\mathbf{9}$ | 0.5874 | 8.78 | 8.800 | 2.579 |
| $\mathbf{1 0}$ | 0.5830 | 9.238 | 9.256 | 2.693 |
| $\mathbf{1 1}$ | 0.5793 | 9.674 | 9.691 | 2.802 |
| $\mathbf{1 2}$ | 0.5760 | 10.092 | 10.108 | 2.906 |
| $\mathbf{1 3}$ | 0.5730 | 10.494 | 10.510 | 3.007 |
| $\mathbf{1 4}$ | 0.5704 | 10.882 | 10.897 | 3.104 |
| $\mathbf{1 5}$ | 0.5681 | 11.257 | 11.271 | 3.197 |
| $\mathbf{1 6}$ | 0.5660 | 11.621 | 11.635 | 3.289 |
| $\mathbf{1 7}$ | 0.5640 | 11.973 | 11.986 | 3.377 |
| $\mathbf{1 8}$ | 0.5622 | 12.314 | 12.327 | 3.462 |
| $\mathbf{1 9}$ | 0.5606 | 12.648 | 12.660 | 3.545 |
| $\mathbf{2 0}$ | 0.5591 | 12.973 | 12.985 | 3.627 |

Table 5: The ratio of area of triangle ABC and CDE

| $\mathbf{c}$ | area ABC | area CDE | $\mathbf{R}_{\mathbf{1}}=\mathbf{C D E} / \mathbf{A B C}$ |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.0691 | 0.9187 | 13.2962 |
| $\mathbf{2}$ | 0.1615 | 0.9579 | 5.9297 |
| $\mathbf{3}$ | 0.2474 | 1.0072 | 4.0717 |
| $\mathbf{4}$ | 0.3260 | 1.0561 | 3.2397 |
| $\mathbf{5}$ | 0.3987 | 1.1029 | 2.7663 |
| $\mathbf{6}$ | 0.4664 | 1.1473 | 2.4599 |
| $\mathbf{7}$ | 0.5303 | 1.1897 | 2.2436 |
| $\mathbf{8}$ | 0.5907 | 1.2301 | 2.0825 |
| $\mathbf{9}$ | 0.6480 | 1.2687 | 1.9581 |
| $\mathbf{1 0}$ | 0.7029 | 1.3059 | 1.8578 |
| $\mathbf{1 1}$ | 0.7556 | 1.3415 | 1.7755 |
| $\mathbf{1 2}$ | 0.8060 | 1.3760 | 1.7071 |
| $\mathbf{1 3}$ | 0.8549 | 1.4092 | 1.6483 |
| $\mathbf{1 4}$ | 0.9022 | 1.4414 | 1.5976 |
| $\mathbf{1 5}$ | 0.9481 | 1.4726 | 1.5532 |
| $\mathbf{1 6}$ | 0.9925 | 1.5032 | 1.5145 |
| $\mathbf{1 7}$ | 1.0358 | 1.5327 | 1.4797 |
| $\mathbf{1 8}$ | 1.0776 | 1.5615 | 1.4491 |
| $\mathbf{1 9}$ | 1.1187 | 1.5896 | 1.4209 |
| $\mathbf{2 0}$ | 1.1586 | 1.6172 | 1.3957 |

Table 6: The ratio of area of triangle ABC and BFG

| $\mathbf{c}$ | area ABC | area BFG | $\mathbf{R}_{\mathbf{2}}=$ BFG/ABC |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.069093 | 1.300454 | 18.8219 |
| $\mathbf{2}$ | 0.161534 | 1.523875 | 9.4338 |
| $\mathbf{3}$ | 0.247362 | 1.720019 | 6.9535 |
| $\mathbf{4}$ | 0.325981 | 1.894057 | 5.8103 |
| $\mathbf{5}$ | 0.398676 | 2.051765 | 5.1464 |
| $\mathbf{6}$ | 0.466397 | 2.196635 | 4.7098 |
| $\mathbf{7}$ | 0.530266 | 2.33199 | 4.3978 |
| $\mathbf{8}$ | 0.590691 | 2.459071 | 4.1630 |
| $\mathbf{9}$ | 0.647951 | 2.578722 | 3.9798 |
| $\mathbf{1 0}$ | 0.702912 | 2.693061 | 3.8313 |
| $\mathbf{1 1}$ | 0.755554 | 2.801913 | 3.7084 |
| $\mathbf{1 2}$ | 0.806045 | 2.906321 | 3.6057 |
| $\mathbf{1 3}$ | 0.854935 | 3.006765 | 3.5170 |
| $\mathbf{1 4}$ | 0.902222 | 3.103746 | 3.4401 |
| $\mathbf{1 5}$ | 0.948093 | 3.197492 | 3.3726 |
| $\mathbf{1 6}$ | 0.992545 | 3.288525 | 3.3132 |
| $\mathbf{1 7}$ | 1.03577 | 3.376523 | 3.2599 |
| $\mathbf{1 8}$ | 1.077571 | 3.461742 | 3.2125 |
| $\mathbf{1 9}$ | 1.118725 | 3.545281 | 3.1690 |
| $\mathbf{2 0}$ | 1.15865 | 3.626554 | 3.1299 |

Table 7: The ratio of area of triangle CDE and BFG

| $\mathbf{c}$ | area CDE | area BFG | $\mathbf{R}_{\mathbf{3}}=\mathbf{B F G} / \mathbf{C D E}$ |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.9187 | 1.3005 | 1.4156 |
| $\mathbf{2}$ | 0.9579 | 1.5239 | 1.5909 |
| $\mathbf{3}$ | 1.0072 | 1.7200 | 1.7078 |
| $\mathbf{4}$ | 1.0561 | 1.8941 | 1.7935 |
| $\mathbf{5}$ | 1.1029 | 2.0518 | 1.8604 |
| $\mathbf{6}$ | 1.1473 | 2.1966 | 1.9146 |
| $\mathbf{7}$ | 1.1897 | 2.3320 | 1.9602 |
| $\mathbf{8}$ | 1.2301 | 2.4591 | 1.9990 |
| $\mathbf{9}$ | 1.2687 | 2.5787 | 2.0325 |
| $\mathbf{1 0}$ | 1.3059 | 2.6931 | 2.0622 |
| $\mathbf{1 1}$ | 1.3415 | 2.8019 | 2.0887 |
| $\mathbf{1 2}$ | 1.3760 | 2.9063 | 2.1121 |
| $\mathbf{1 3}$ | 1.4092 | 3.0068 | 2.1337 |
| $\mathbf{1 4}$ | 1.4414 | 3.1037 | 2.1533 |
| $\mathbf{1 5}$ | 1.4726 | 3.1975 | 2.1713 |
| $\mathbf{1 6}$ | 1.5032 | 3.2885 | 2.1877 |
| $\mathbf{1 7}$ | 1.5327 | 3.3765 | 2.2030 |
| $\mathbf{1 8}$ | 1.5615 | 3.4617 | 2.2170 |
| $\mathbf{1 9}$ | 1.5896 | 3.5453 | 2.2304 |
| $\mathbf{2 0}$ | 1.6172 | 3.6266 | 2.2426 |

Table 8: The hypotenuse values and their ratios

| $\mathbf{c}$ | $\mathbf{A C}$ | $\mathbf{C E}$ | $\mathbf{R}_{\mathbf{4}}=\mathbf{C E} / \mathbf{A C}$ |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.6797 | 2.9591 | 4.3539 |
| $\mathbf{2}$ | 1.2132 | 3.3717 | 2.7792 |
| $\mathbf{3}$ | 1.6618 | 3.7215 | 2.2394 |
| $\mathbf{4}$ | 2.0552 | 4.0289 | 1.9603 |
| $\mathbf{5}$ | 2.4103 | 4.3060 | 1.7865 |
| $\mathbf{6}$ | 2.7357 | 4.5602 | 1.6669 |
| $\mathbf{7}$ | 3.0394 | 4.7970 | 1.5783 |
| $\mathbf{8}$ | 3.3243 | 5.0192 | 1.5099 |
| $\mathbf{9}$ | 3.5923 | 5.2288 | 1.4555 |
| $\mathbf{1 0}$ | 3.8485 | 5.4285 | 1.4105 |
| $\mathbf{1 1}$ | 4.0928 | 5.6185 | 1.3728 |
| $\mathbf{1 2}$ | 4.3262 | 5.8016 | 1.3410 |
| $\mathbf{1 3}$ | 4.5516 | 5.9767 | 1.3131 |
| $\mathbf{1 4}$ | 4.7691 | 6.1460 | 1.2887 |
| $\mathbf{1 5}$ | 4.9797 | 6.3094 | 1.2670 |
| $\mathbf{1 6}$ | 5.1832 | 6.4688 | 1.2480 |
| $\mathbf{1 7}$ | 5.3809 | 6.6223 | 1.2307 |
| $\mathbf{1 8}$ | 5.5715 | 6.7718 | 1.2154 |
| $\mathbf{1 9}$ | 5.7592 | 6.9174 | 1.2011 |
| $\mathbf{2 0}$ | 5.9409 | 7.0599 | 1.1884 |

## REFERENCES

1. Cameron.J.M (1952): Tables for constructing and for computing characteristics of single sampling plan, Industrial Quality Control.9, 37-39.
2. Carroll W. M. J (1963): Application of an Inspection Scheme for attributes, Ph.D Thesis.
3. Douglas C Montgomery (2001): Introduction to Statistical Quality Control, $4^{\text {th }}$ Edition, Arizona State University.
4. Lilly Christina. A (1989): Sampling Inspection Plans indexed by Inflection point a review, M.phil contributed to Bharathiar University, Coimbatore, Tamilnadu, India.
5. Soundararajan. V (1975): Maximum Allowable Percent Defective (MAPD) Single Sampling Inspection by Attributes Plan, Journal of Quality Technology, Vol. 7 No.4, 173-182
6. Suresh .K.K and Ramkumar .T.B (1996): selection of sampling Plans indexed with Maximum Allowable Average Outgoing Quality.
7. Suresh K.K (1993): A study on Acceptance Sampling using Acceptable Quality Levels. Ph.D Thesis Bharathiar University, Coimbatore, Tamilnadu, India.
